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# Heat and mass transfer during the sump development in a potash solution mine

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#### **Appendix A: Derivation of Rectangular Interior Node**

$$\frac{\partial^2 T}{\partial x^2} = \frac{T_2 + T_4 - 2T_0}{a^2}$$

$$\frac{\partial^2 T}{\partial y^2} = \frac{T_1 + T_3 - 2T_0}{b^2}$$

$$\frac{\partial^{2} T}{\partial x^{2}} + \frac{\partial^{2} T}{\partial y^{2}} = \frac{T_{2} + T_{4} - 2T_{0}}{a^{2}} + \frac{T_{1} + T_{3} - 2T_{0}}{b^{2}}$$

$$\frac{\partial^{2}T}{\partial x^{2}} + \frac{\partial^{2}T}{\partial y^{2}} = \frac{b^{2}(T_{2} + T_{4} - 2T_{0}) + a^{2}(T_{1} + T_{3} - 2T_{0})}{b^{2}a^{2}}$$
$$\frac{\partial^{2}T}{\partial x^{2}} + \frac{\partial^{2}T}{\partial y^{2}} = \frac{b^{2}(T_{2} + T_{4}) + a^{2}(T_{1} + T_{3}) - 2T_{0}(b^{2} + a^{2})}{b^{2}a^{2}}$$

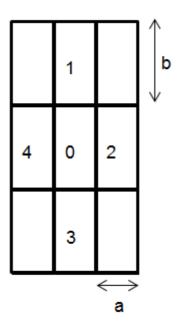
$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} = 0$$
 Therefore;

$$b^{2}(T_{2} + T_{4}) + a^{2}(T_{1} + T_{3}) - 2T_{0}(b^{2} + a^{2}) = 0$$

$$T_0 = \frac{b^2 (T_2 + T_4) + a^2 (T_1 + T_3)}{2(b^2 + a^2)}$$

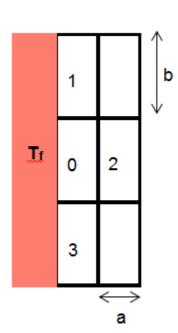
## **Appendix B: FDM Equations for Rectangular Nodes Interior Nodes**

$$T_0 = \frac{b^2 (T_2 + T_4) + a^2 (T_1 + T_3)}{2(b^2 + a^2)}$$



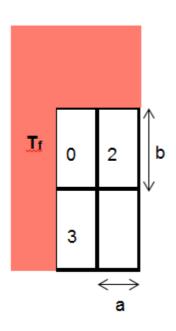
#### **Isothermal Boundary Layer**

$$T_{0} = \left(\frac{T_{1}}{2} + T_{2} + \frac{T_{3}}{2} + \frac{ha}{\lambda}T_{f}\right) \frac{1}{2 + \frac{ha}{\lambda}}$$



#### **External Corner Node**

$$T_0 = \left(\frac{T_2}{2} + \frac{T_3}{2} + \frac{ha}{\lambda}T_f\right) \frac{1}{1 + \frac{ha}{\lambda}}$$



#### **Appendix C: Depth Calculation**

$$y = 5e-6x^2 + 0.0031x + 292.67$$

When y= 328

$$328 = 5e-6x^2 + 0.0031x + 292.67$$

$$0 = 5e-6x^2 + 0.0031x - 35.33$$

Using the quadratic equation:

$$x = \frac{-0.0031 + \sqrt{(0.0031)^2 - (4 \cdot 5e - 6 \cdot -35.33)}}{2 \cdot 0.0031}$$

$$x = 2366.21 \text{ m}$$

#### **Appendix D: Equating of Heat Transfer Equations**

$$\dot{Q} = h\Delta T_{SL}ac$$

$$T_{_{b}} = T_{_{t}} - \frac{\overset{\cdot}{Q} \Delta z}{\rho C_{_{p}} u V} \text{ therefore } \overset{\cdot}{Q} = \frac{\Delta T_{_{tb}} \rho C_{_{p}} u V}{\Delta z}$$

Equating the two equations gives;

$$\begin{split} \frac{\Delta T_{tb} \rho C_{p} u V}{\Delta z} &= h \Delta T_{SL} ac \\ \frac{\Delta T_{tb} \rho C_{p} u V}{\Delta z hac} &= \Delta T_{SL} \end{split}$$

### Appendix E: Fluid Properties

Fluid	Density	Prandtl	Thermal	Viscosity	Specific	Reference
	(kg/m³)	Number	Conductivity	(pa.s)	Heat	
			(W/mK)		Capacity	
					(J/kgK)	
Water	1000	9.29	0.59	0.001002	4193	Haywood,
						1990
Brine	1076.8	9.29	0.59	0.001002	4193	Haywood,19
						90 and Lide,
						2004
Diesel	820.8	27.74	0.14	0.012	1914.21	Chemical
						Hazards
						Response
						Information
						System,
						cited in Zen-
						Stoves, 1999
Gasoline	704.01	6.68	0.88	0.00041	2055.72	Chemical
						Hazards
						Response
						Information
						System,
						cited in Zen-
						Stoves, 1999
Naphtha	849.94	73.13	0.15	0.0055	2001.29	Chemical
						Hazards
						Response
						Information
						System,
						cited in Zen-
						Stoves, 1999
Kerosene	793.87	17.22	0.13	0.0011	1963.61	Chemical
						Hazards
						Response

			Information
			System,
			cited in Zen-
			Stoves, 1999

All properties taken at 20°C and 12% KCl by mass in water.